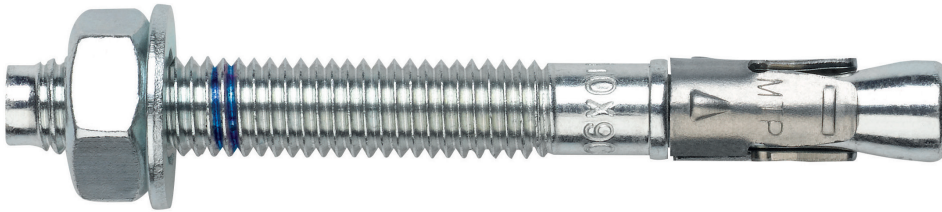




## Through-bolt expansion anchor with controlled torque, for use in cracked and non cracked concrete

**MTP**

ETA Assessed Option 1. Zinc-plated shaft. A4 Stainless clip.



## PRODUCT INFORMATION

### DESCRIPTION

Metallic anchor, with male thread, expansion by controlled torque.

### OFFICIAL DOCUMENTATION

- AVCP-1219-CPR-0053.
- ETA 12/0397 option 1.
- Declaration of Performance DoP MTP.

### SIZES

M8x50 to M24x235.

### DESIGN LOAD RANGE

From 5,00 to 33,3 kN [non cracked].  
From 2,7 to 20,0 kN [cracked].



### BASE MATERIAL

Concrete class from C20/25 to C50/60  
cracked or non-cracked.



Stone



Concrete



Reinforced Concrete



Cracked Concrete

### ASSESSMENTS

- Option 1 [Cracked and non-cracked concrete]
- Fire Resistance R30-120
- Seismic C1 M10 ÷ M16
- Seismic C2 M12 ÷ M16



12  
Técnicas Expansivas S.L.  
Segador 13. Logroño. Spain  
ETA 12/0397  
1219  
Structural fixings in concrete

FIRE  
RESISTANCESEISMIC  
C2 & C1

### CHARACTERISTICS AND BENEFITS

- Easy installation.
- Use in cracked and non-cracked concrete.
- Use for medium-heavy duty loads.
- Pre-installation or through the drill-hole of the fixture.
- Variety of lengths and diameters: flexibility in assembly.
- For static and quasi-static loads.
- Available at INDEXcal.



### MATERIALS

Shaft: Cold-formed steel, zinc-plated  $\geq 5 \mu\text{m}$ .

Washer: DIN 125 or DIN 9021, zinc-plated  $\geq 5 \mu\text{m}$ .

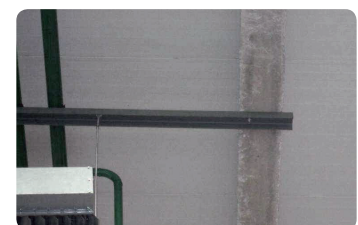
Nut: DIN 934, zinc-plated  $\geq 5 \mu\text{m}$ .

Clip: A4 Stainless steel



### APPLICATIONS

- Anchor plates.
- Metallic structures.
- Bridges.
- Urban fitments.
- Protective fences.
- Catenaries.
- Elevators.
- Pipe supports.





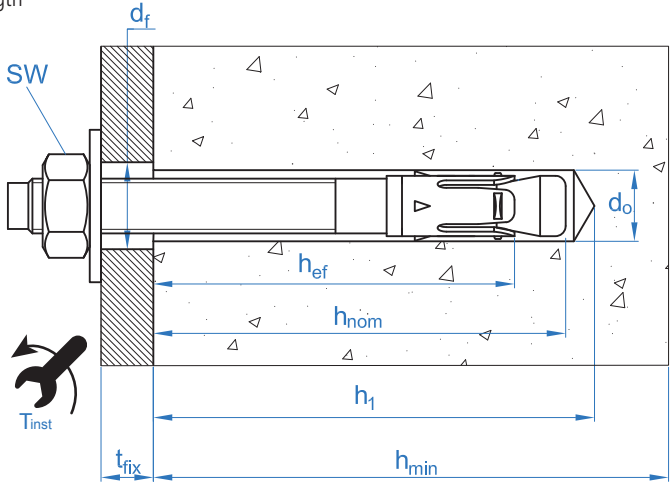
**MECHANICAL PROPERTIES**

			M8	M10	M12	M16	M20	M24
<b>Cone area section</b>								
$A_s$	(mm <sup>2</sup> )	Cone area section	22,9	41,8	55,4	103,9	176,7	298,6
$f_{u,s}$	(N/mm <sup>2</sup> )	Characteristic tension resistance	790	750	730	700	660	600
$f_{y,s}$	(N/mm <sup>2</sup> )	Yield strength	632	600	585	560	530	480
<b>Threaded area section</b>								
$A_s$	(mm <sup>2</sup> )	Cone area section	36,6	58,0	84,3	157,0	245,0	353,0
$f_{u,s}$	(N/mm <sup>2</sup> )	Characteristic tension resistance	600	600	600	600	600	600
$f_{y,s}$	(N/mm <sup>2</sup> )	Yield Strength	480	480	480	480	480	480

**INSTALLATION DATA**

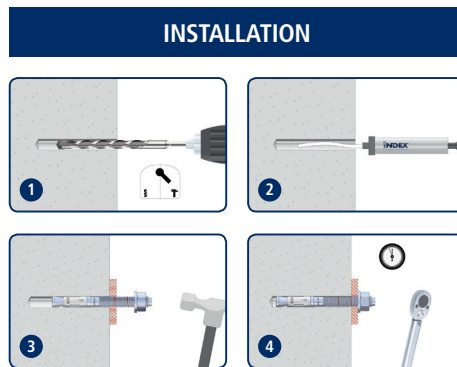
SIZE			M8	M10	M12	M16	M20	M24
Code			AP08XXX	AP10XXX	AP12XXX	AP16XXX	AP20XXX	AP24XXX
$d_0$	Nominal diameter of drill bit	[mm]	8	10	12	16	20	24
$T_{ins}$	Installation torque moment	[Nm]	20	40	60	100	200	250
$d_{f\leq}$	Diameter of clearance hole in the fixture	[mm]	9	12	14	18	22	26
$h_1$	Minimum drill hole depth	[mm]	60	75	85	105	125	155
$h_{nom}$	Installation depth	[mm]	55	68	80	97	114	143
$h_{ef}$	Effective embedment depth	[mm]	48	60	70	85	100	125
$h_{min}$	Minimum base material thickness	[mm]	100	120	140	170	200	250
$t_{fix}$	Maximum thickness of fixture	[mm]	L - 66	L - 80	L - 96	L - 117	L-138	L-170
$s_{cr,N}$	Critical spacing	[mm]	144	180	210	255	300	375
$c_{cr,N}$	Critical edge distance	[mm]	72	90	105	128	150	188
$s_{cr,sp}$	Critical distance (splitting)	[mm]	288	300	350	425	500	560
$c_{cr,sp}$	Critical edge distance (splitting)	[mm]	144	150	175	213	250	280
$s_{min}$	Minimum spacing	[mm]	50	60	70	85	100	125
$c_{min}$	Minimum edge distance	[mm]	50	60	70	85	100	125
SW	Installation wrench		13	17	19	24	30	30

\*L = Total anchor length





Code	INSTALLATION PRODUCTS
	Hammer drill
BHDSXXXXX	Concrete Drill bits
MOBOMBA	Blow pump
MORCEPKIT	Cleaning Brush
DOMTAXX	Installation hammering tool
	Torque wrench
	Hexagonal socket



## Resistances in C20/25 concrete for an isolated anchor, without effects of edge distance or spacing

Characteristic Resistance $N_{Rk}$ and $V_{Rk}$															
TENSION							SHEAR								
Size		M8	M10	M12	M16	M20	M24	Size		M8	M10	M12	M16	M20	M24
$N_{Rk}$	Non-cracked concrete [kN]	9,0	16,0	20,0	35,0	50,0	50,0	$V_{Rk}$	Non-cracked concrete [kN]	11,0	17,4	25,3	47,1	73,1	84,7
$N_{Rk}$	Cracked concrete [kN]	5,0	9,0	12,0	25,0	30,0	30,0	$V_{Rk}$	Cracked concrete [kN]	11,0	17,4	25,3	47,1	73,1	84,7

Design Resistance $N_{Rd}$ and $V_{Rd}$															
TENSION							SHEAR								
Size		M8	M10	M12	M16	M20	M24	Size		M8	M10	M12	M16	M20	M24
$N_{Rd}$	Non-cracked concrete [kN]	5,0	10,6	13,3	23,3	33,3	27,7	$V_{Rd}$	Non-cracked concrete [kN]	8,8	13,9	20,2	37,6	58,4	67,7
$N_{Rd}$	Cracked concrete [kN]	2,7	6,0	8,0	16,6	20,0	16,6	$V_{Rd}$	Cracked concrete [kN]	8,8	13,9	20,2	37,6	58,4	67,7

Maximum Loads Recommended $N_{rec}$ and $V_{rec}$															
TENSION							SHEAR								
Size		M8	M10	M12	M16	M20	M24	Size		M8	M10	M12	M16	M20	M24
$N_{rec}$	Non-cracked concrete [kN]	3,5	7,6	9,5	16,6	23,8	19,8	$V_{rec}$	Non-cracked concrete [kN]	6,3	9,9	14,4	26,9	41,7	48,4
$N_{rec}$	Cracked concrete [kN]	2,0	4,2	5,7	11,9	14,2	11,9	$V_{rec}$	Cracked concrete [kN]	6,3	9,9	14,4	26,9	41,7	48,4

## Simplified calculation method

### European Technical Assessment ETA 12/0397

Simplified version of the calculation method according to ETAG 001, annex C. Resistance is calculated according to the data shown in assessment ETA 12/0397.

- Influence of concrete strength.
- Influence of edge distance.
- Influence of spacing between anchors.
- Influence of reinforcements.
- Influence of base material thickness.
- Influence of load application angle.
- Valid for a group of two anchors.

The calculation method is based on the following simplification: **Different loads do not act on individual anchors, without eccentricity.**



### INDEXcal

For a more accurate calculation and to take more constructive provisions into account, we recommend using our calculation program INDEXcal. It may be easily downloaded from our website [www.indexfix.com](http://www.indexfix.com)

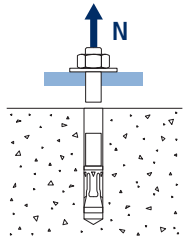


# MTP

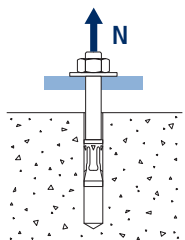
## TENSION LOADS

- Steel design resistance:  $N_{Rd,s}$
- Pull-out design resistance:  $N_{Rd,p} = N_{Rd,p}^o \cdot \Psi_c$
- Concrete cone design resistance:  $N_{Rd,c} = N_{Rd,c}^o \cdot \Psi_b \cdot \Psi_{s,N} \cdot \Psi_{c,N} \cdot \Psi_{re,N}$
- Concrete splitting design resistance:  $N_{Rd,sp} = N_{Rd,c}^o \cdot \Psi_b \cdot \Psi_{s,sp} \cdot \Psi_{c,sp} \cdot \Psi_{re,N} \cdot \Psi_{h,sp}$

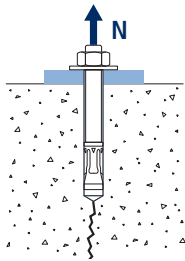
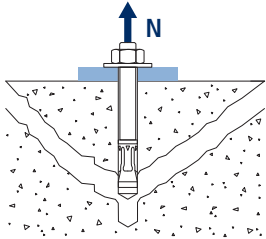
Steel Design resistance							
$N_{Rd,s}$							
Size		M8	M10	M12	M16	M20	M24
$N_{Rd}^o$	[kN]	12,1	20,9	26,9	48,5	77,7	119,5



Pull-out design resistance							
$N_{Rd,p} = N_{Rd,p}^o \cdot \Psi_c$							
Size		M8	M10	M12	M16	M20	M24
$N_{Rd,p}^o$	Non-cracked concrete [kN]	5,0	10,6	13,3	23,3	33,3	27,7
$N_{Rd,p}^o$	Cracked concrete [kN]	2,7	6,0	8,0	16,6	20,0	16,6



Concrete cone design resistance							
$N_{Rd,c} = N_{Rd,c}^o \cdot \Psi_b \cdot \Psi_{s,N} \cdot \Psi_{c,N} \cdot \Psi_{re,N}$							
Concrete splitting design resistance*							
$N_{Rd,sp} = N_{Rd,c}^o \cdot \Psi_b \cdot \Psi_{s,sp} \cdot \Psi_{c,sp} \cdot \Psi_{re,N} \cdot \Psi_{h,sp}$							
Size		M8	M10	M12	M16	M20	M24
$N_{Rd,c}^o$	Non-cracked concrete [kN]	9,3	15,6	19,6	26,3	33,6	39,1
$N_{Rd,c}^o$	Cracked concrete [kN]	6,6	11,1	14,0	18,8	24,0	27,9



\*Concrete splitting design resistance must only be considered for non-cracked concrete.

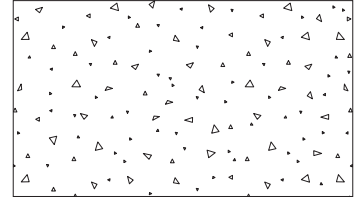


MTP

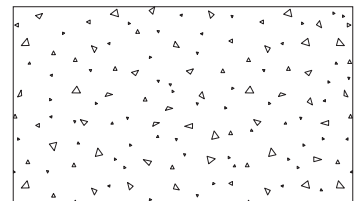
## Coefficients of influence

Influence of concrete strength resistance in pul-out failure  $\Psi_c$ 

		M8	M10	M12	M16	M20	M24
$\Psi_c$	C 20/25	1,00	1,00	1,00	1,00	1,00	1,00
	C 30/37	1,22	1,16	1,22	1,22	1,16	1,22
	C 40/50	1,41	1,31	1,41	1,41	1,31	1,41
	C 50/60	1,55	1,41	1,55	1,55	1,41	1,55

Influence of concrete strength in concret cone and splitting failure  $\Psi_b$ 

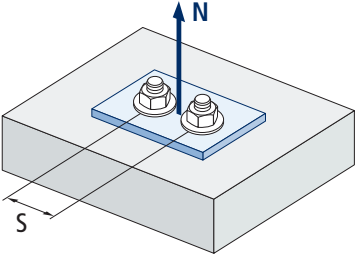
		M8	M10	M12	M16	M20	M24
$\Psi_b$	C 20/25	1,00					
	C 30/37	1,22					
	C 40/50	1,41					
	C 50/60	1,55					



$$\Psi_b = \sqrt{\frac{f_{ck,cube}}{25}} \geq 1$$



**MTP**



$$\psi_{s,N} = 0,5 + \frac{s}{2 \cdot s_{cr,N}} \leq 1$$

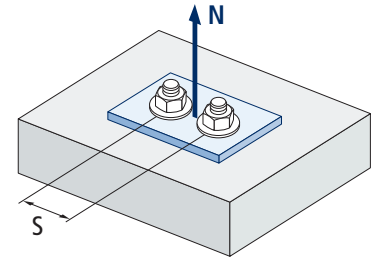
Influence of spacing (concrete cone) $\psi_{s,N}$						
s [mm]	MTP					
	M8	M10	M12	M16	M20	M24
50	0,67					
55	0,69					
60	0,71	0,67				
65	0,73	0,68				
70	0,74	0,69	0,67			
80	0,78	0,50	0,50			
85	0,80	0,74	0,70	0,67		
90	0,81	0,75	0,71	0,68		
100	0,85	0,78	0,74	0,70	0,67	
105	0,86	0,79	0,75	0,71	0,68	
110	0,88	0,81	0,76	0,72	0,68	
120	0,92	0,83	0,79	0,74	0,70	
125	0,93	0,85	0,80	0,75	0,71	0,67
126	0,94	0,85	0,80	0,75	0,71	0,67
128	0,94	0,86	0,80	0,75	0,71	0,67
130	0,95	0,86	0,81	0,75	0,72	0,67
135	0,97	0,88	0,82	0,76	0,73	0,68
144	1,00	0,90	0,84	0,78	0,74	0,69
150		0,92	0,86	0,79	0,75	0,70
165		0,96	0,89	0,82	0,78	0,72
170		0,97	0,90	0,83	0,78	0,73
180		1,00	0,93	0,85	0,80	0,74
195			0,96	0,88	0,83	0,76
200			0,98	0,89	0,83	0,77
210			1,00	0,91	0,85	0,78
220				0,93	0,87	0,79
225				0,94	0,88	0,80
252				0,99	0,92	0,84
255				1,00	0,93	0,84
260					0,93	0,85
300					1,00	0,90
309						0,91
310						0,91
375						1,00

Value without reduction = 1



Influence of spacing (concrete splitting) $\psi_{s,sp}$						
s [mm]	MTP					
	M8	M10	M12	M16	M20	M24
50	0,59					
55	0,60					
60	0,60	0,60				
65	0,61	0,61				
70	0,62	0,62	0,60			
80	0,64	0,63	0,61			
85	0,65	0,64	0,62	0,60		
90	0,66	0,65	0,63	0,61		
100	0,67	0,67	0,64	0,62	0,60	
110	0,69	0,68	0,66	0,63	0,61	
125	0,72	0,71	0,68	0,65	0,63	0,61
128	0,72	0,71	0,68	0,65	0,63	0,61
135	0,73	0,73	0,69	0,66	0,64	0,62
140	0,74	0,73	0,70	0,66	0,64	0,63
150	0,76	0,75	0,71	0,68	0,65	0,63
160	0,78	0,77	0,73	0,69	0,66	0,64
165	0,79	0,78	0,74	0,69	0,67	0,65
168	0,79	0,78	0,74	0,70	0,67	0,65
180	0,81	0,80	0,76	0,71	0,68	0,66
192	0,83	0,82	0,77	0,73	0,69	0,67
200	0,85	0,83	0,79	0,74	0,70	0,68
210	0,86	0,85	0,80	0,75	0,71	0,69
220	0,88	0,87	0,81	0,76	0,72	0,70
260	0,95	0,93	0,87	0,81	0,76	0,73
288	1,00	0,98	0,91	0,84	0,79	0,76
300		1,00	0,93	0,85	0,80	0,77
336			0,98	0,90	0,84	0,80
350			1,00	0,91	0,85	0,81
412				0,98	0,91	0,87
425				1,00	0,93	0,88
500	Value without reduction = 1				1,00	0,95
510						0,96
560						1,00

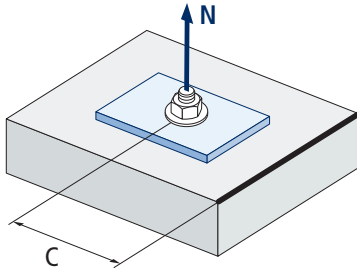
MTP



$$\psi_{s,sp} = 0,5 + \frac{s}{2 \cdot s_{cr,sp}} \leq 1$$



**MTP**



$$\psi_{c,sp} = 0,35 + \frac{0,5 \cdot c}{C_{cr,sp}} + \frac{0,15 \cdot c^2}{C_{cr,sp}^2} \leq 1$$

Influence of concrete edge distance (splitting) $\psi_{c,sp}$						
c [mm]	MTP					
	M8	M10	M12	M16	M20	M24
50	0,54					
60	0,58	0,57				
65	0,61	0,59				
70	0,63	0,62	0,57			
75	0,65	0,64	0,59			
80	0,67	0,66	0,61			
83	0,69	0,67	0,62			
84	0,69	0,68	0,62			
85	0,70	0,68	0,63	0,57		
90	0,72	0,70	0,65	0,59		
96	0,75	0,73	0,67	0,61		
100	0,77	0,75	0,68	0,62	0,57	
105	0,79	0,77	0,70	0,63	0,59	
110	0,82	0,80	0,72	0,65	0,60	
125	0,90	0,87	0,78	0,70	0,64	0,60
128	0,91	0,89	0,80	0,70	0,65	0,61
130	0,92	0,90	0,80	0,71	0,65	0,61
135	0,95	0,92	0,82	0,73	0,66	0,63
144	1,00	0,97	0,86	0,76	0,69	0,65
150		1,00	0,89	0,78	0,70	0,66
168			0,97	0,84	0,75	0,70
175			1,00	0,86	0,77	0,72
180				0,88	0,79	0,73
206				0,97	0,86	0,80
213				1,00	0,88	0,82
250	Value without reduction = 1				1,00	0,92
255						0,93
280						1,00

Invalid value

Value without reduction = 1



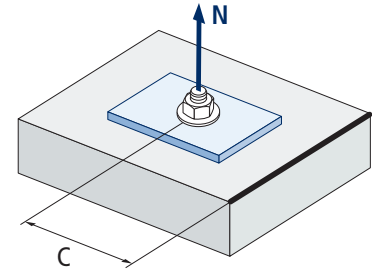


Influence of concrete edge distance (concrete cone) $\Psi_{c,N}$						
c [mm]	MTP					
	M8	M10	M12	M16	M20	M24
50	0,77					
53	0,80					
60	0,87	0,75				
63	0,90	0,77				
65	0,92	0,79				
70	0,98	0,83	0,75			
72	1,00	0,85	0,76			
75		0,87	0,78			
80		0,91	0,82			
83		0,94	0,84			
85		0,96	0,85	0,75		
90		1,00	0,89	0,78		
98			0,95	0,82		
100			0,96	0,83	0,75	
105			1,00	0,86	0,77	
110				0,89	0,80	
113				0,91	0,81	
125				0,98	0,87	0,75
126				0,99	0,88	0,75
128				1,00	0,89	0,76
135					0,92	0,79
150					1,00	0,84
155						0,86
188						1,00

**Invalid value**

**Value without reduction = 1**

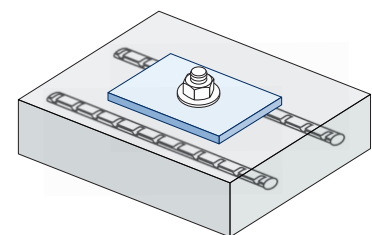
**MTP**



$$\Psi_{c,N} = 0,35 + \frac{0,5 \cdot c}{c_{cr,N}} + \frac{0,15 \cdot c^2}{c_{cr,N}^2} \leq 1$$

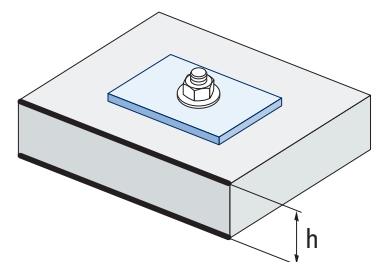
Influence of reinforcements $\Psi_{re,N}$						
$\Psi_{re,N}$	MTP					
	M8	M10	M12	M16	M20	M24
	0,74	0,80	0,85	0,93	1,00	1,00

\*This factor only applies for a high density of reinforcements. If in the area of the anchor there are reinforcements with a distancing of  $\geq 150$  mm (any diameter) or with a diameter  $\leq 10$  mm and a distancing of  $\geq 100$  mm, a  $f_{re,N} = 1$  factor may be applied.



$$\Psi_{re,N} = 0,5 + \frac{h_{ef}}{200} \leq 1$$

Influence of base material thickness $\Psi_{h,sp}$											
$\Psi_{h,sp}$	MTP										
	h/h <sub>ef</sub>	2,00	2,20	2,40	2,60	2,80	3,00	3,20	3,40	3,60	$\geq 3,68$
	$\Psi_{h,sp}$	1,00	1,07	1,13	1,19	1,25	1,31	1,37	1,42	1,48	1,50



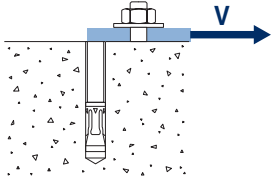
$$\Psi_{h,sp} = \left( \frac{h}{2 \cdot h_{ef}} \right)^{2/3} \leq 1,5$$

# MTP

## SHEAR LOADS

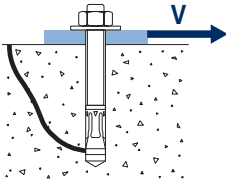
- Steel design resistance without lever arm:  $V_{Rd,s}$
- Pry-out design resistance:  $V_{Rd,cp} = k \cdot N_{Rd,c}^o$
- Concrete edge design resistance:  $V_{Rd,c} = V_{Rd,c}^o \cdot \psi_b \cdot \psi_{se,V} \cdot \psi_{c,V} \cdot \psi_{re,V} \cdot \psi_{\alpha,V} \cdot \psi_{h,V}$

Steel design resistance							
$V_{Rd,s}$							
Size		M8	M10	M12	M16	M20	M24
$V_{Rd,s}$	[kN]	8,8	13,9	20,2	37,6	58,8	67,7

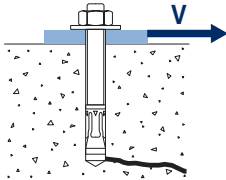


Pry-out design resistance*							
$V_{Rd,cp} = k \cdot N_{Rd,c}^o$							
Size		M8	M10	M12	M16	M20	M24
k		1	2	2	2	2	2

\*  $N_{Rd,c}^o$  Concrete cone design resistance for tension loads



Concrete edge resistance								
$V_{Rd,c} = V_{Rd,c}^o \cdot \psi_b \cdot \psi_{se,V} \cdot \psi_{c,V} \cdot \psi_{re,V} \cdot \psi_{\alpha,V} \cdot \psi_{h,V}$								
Size		M8	M10	M12	M16	M20	M24	
$V_{Rd,c}^o$	Non-cracked concrete	[kN]	6,2	8,9	11,5	15,9	20,8	30,1
	Cracked concrete	[kN]	4,4	6,3	8,2	11,3	14,7	21,4





MTP

## Coefficients of influence

Influence of concrete strength in concrete edge failure  $\Psi_b$ 

		M8	M10	M12	M16	M20	M24	
$\Psi_b$	C 20/25	1,00						
	C 30/37	1,22						
	C 40/50	1,41						
	C 50/60	1,55						



$$\Psi_b = \sqrt{\frac{f_{ck,cube}}{25}} \geq 1$$

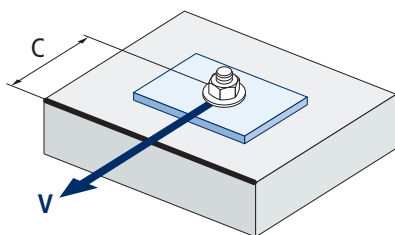
Influence of edge distance and spacing  $\Psi_{se,V}$ 

FOR ONE ANCHOR ONLY

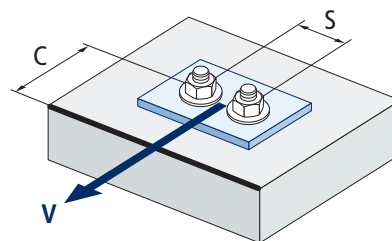
$c/h_{ef}$	0,50	0,75	1,00	1,25	1,50	1,75	2,00	2,25	2,50	2,75	3,00	3,25	3,50	3,75	4,00	4,50	5,00
Isolated	0,35	0,65	1,00	1,40	1,84	2,32	2,83	3,38	3,95	4,56	5,20	5,86	6,55	7,26	8,00	9,55	11,18

FOR TWO ANCHORS

$c/h_{ef}$	0,50	0,75	1,00	1,25	1,50	1,75	2,00	2,25	2,50	2,75	3,00	3,25	3,50	3,75	4,00	4,50	5,00	
s/c	1,0	0,24	0,43	0,67	0,93	1,22	1,54	1,89	2,25	2,64	3,04	3,46	3,91	4,37	4,84	5,33	6,36	7,45
	1,5	0,27	0,49	0,75	1,05	1,38	1,74	2,12	2,53	2,96	3,42	3,90	4,39	4,91	5,45	6,00	7,16	8,39
	2,0	0,29	0,54	0,83	1,16	1,53	1,93	2,36	2,81	3,29	3,80	4,33	4,88	5,46	6,05	6,67	7,95	9,32
	2,5	0,32	0,60	0,92	1,28	1,68	2,12	2,59	3,09	3,62	4,18	4,76	5,37	6,00	6,66	7,33	8,75	10,25
	≥3,0	0,35	0,65	1,00	1,40	1,84	2,32	2,83	3,38	3,95	4,56	5,20	5,86	6,55	7,26	8,00	9,55	11,18



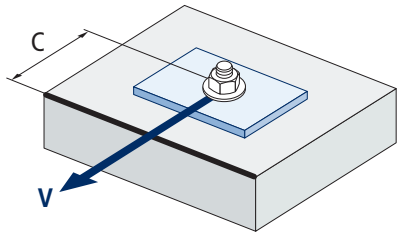
$$\Psi_{se,V} = \left(\frac{c}{h_{ef}}\right)^{1,5}$$



$$\Psi_{se,V} = \left(\frac{c}{h_{ef}}\right)^{1,5} \cdot \left(1 + \frac{s}{3 \cdot c}\right) \cdot 0,5 \leq \left(\frac{c}{h_{ef}}\right)^{1,5}$$



**MTP**

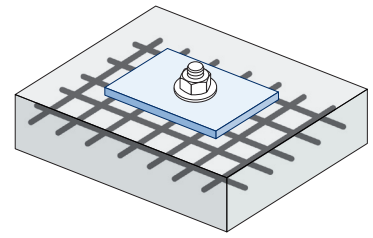


$$\psi_{c,v} = \left( \frac{d}{c} \right)^{0,20}$$

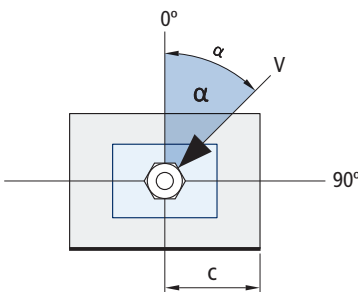
Influence of concrete edge distance $\psi_{c,v}$						
c [mm]	MTP					
	M8	M10	M12	M16	M20	M24
40						
45						
50	0,69					
55	0,68					
60	0,67	0,70				
65	0,66	0,69	0,71			
70	0,65	0,68	0,70			
80	0,63	0,66	0,68			
85	0,62	0,65	0,68	0,72		
90	0,62	0,64	0,67	0,71		
100	0,60	0,63	0,65	0,69	0,72	
105	0,60	0,62	0,65	0,69	0,72	
110	0,59	0,62	0,64	0,68	0,71	
120	0,58	0,61	0,63	0,67	0,70	
125	0,58	0,60	0,63	0,66	0,69	0,72
130	0,57	0,60	0,62	0,66	0,69	0,71
135	0,57	0,59	0,62	0,65	0,68	0,71
140	0,56	0,59	0,61	0,65	0,68	0,70
150	0,56	0,58	0,60	0,64	0,67	0,69
160	0,55	0,57	0,60	0,63	0,66	0,68
170	0,54	0,57	0,59	0,62	0,65	0,68
175	0,54	0,56	0,59	0,62	0,65	0,67
180	0,54	0,56	0,58	0,62	0,64	0,67
190	0,53	0,55	0,58	0,61	0,64	0,66
200	0,53	0,55	0,57	0,60	0,63	0,65
210	0,52	0,54	0,56	0,60	0,62	0,65
220	0,52	0,54	0,56	0,59	0,62	0,64
230	0,51	0,53	0,55	0,59	0,61	0,64
240	0,51	0,53	0,55	0,58	0,61	0,63
250	0,50	0,53	0,54	0,58	0,60	0,63
260	0,50	0,52	0,54	0,57	0,60	0,62
270	0,49	0,52	0,54	0,57	0,59	0,62
280	0,49	0,51	0,53	0,56	0,59	0,61
290	0,49	0,51	0,53	0,56	0,59	0,61
300	0,48	0,51	0,53	0,56	0,58	0,60



Influence of reinforcements $\Psi_{re,v}$			
	Without perimetral reinforcements	Perimetral reinforcements $\geq \text{Ø}12 \text{ mm}$	Perimetral reinforcements with brackets $\leq 100 \text{ mm}$
Non-cracked concrete	1	1	1
Cracked concrete	1	1,2	1,4

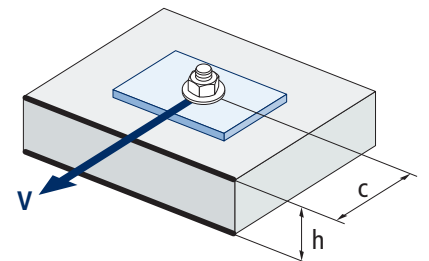


Influence of load application angle $\Psi_{\alpha,v}$											
Angle, $\alpha(^{\circ})$	0°	10°	20°	30°	40°	50°	60°	70°	80°	90°	
$\Psi_{\alpha,v}$	1,00	1,01	1,05	1,13	1,24	1,40	1,64	1,97	2,32	2,50	



$$\Psi_{\alpha,v} = \sqrt{\frac{1}{(\cos \alpha_v)^2 + \left(\frac{\sin \alpha_v}{2,5}\right)^2}} \geq 1$$

Influence of base material thickness $\Psi_{h,v}$											
		MTP									
h/c	0,15	0,30	0,45	0,60	0,75	0,90	1,05	1,20	1,35	$\geq 1,5$	
$\Psi_{h,v}$	0,32	0,45	0,55	0,63	0,71	0,77	0,84	0,89	0,95	1,00	



$$\Psi_{h,v} = \left(\frac{h}{1,5 \cdot c}\right)^{0,5} \geq 1,0$$



# MTP

## FIRE RESISTANCE

Characteristic Resistance*												
	TENSION						SHEAR					
	M8	M10	M12	M16	M20	M24	M8	M10	M12	M16	M20	M24
RF30	0,4	0,9	1,7	3,1	4,9	7,1	0,4	0,9	1,7	3,1	4,9	7,1
RF60	0,3	0,8	1,3	2,4	3,7	5,3	0,3	0,8	1,3	2,4	3,7	5,3
RF90	0,3	0,6	1,1	2,0	3,2	4,6	0,3	0,6	1,1	2,0	3,2	4,5
RF120	0,2	0,5	0,8	1,6	2,5	3,5	0,2	0,5	0,8	1,6	2,5	3,5

\*The safety factor for design resistance under fire exposure is  $\gamma_{M,fi}=1$  (in absence of other national regulations). As a result the Characteristic Resistance is the same as Design Resistance.

Maximum Load Recommended												
	TENSION						SHEAR					
	M8	M10	M12	M16	M20	M24	M8	M10	M12	M16	M20	M24
RF30	0,3	0,6	1,2	2,2	3,5	5,1	0,3	0,6	1,2	2,2	3,5	5,1
RF60	0,2	0,6	0,9	1,7	2,6	3,8	0,2	0,6	0,9	1,7	2,6	3,8
RF90	0,2	0,4	0,8	1,4	2,3	3,3	0,2	0,4	0,8	1,4	2,3	3,2
RF120	0,1	0,4	0,6	1,1	1,8	2,5	0,1	0,4	0,6	1,1	1,8	2,5

## RANGE

Code	Seismic assessment	Size	Maximum thickness of fixture	Axle letter (length)			Code	Seismic assessment	Size	Maximum thickness of fixture	Axle letter (length)		
• AP08050	-	M8 x 50 Ø8	2	A	100	800	AP12120	C1&C2	M12 x 120 Ø12	24	G	50	200
AP08075	-	M8 x 75 Ø8	9	C	100	600	AP12130	C1&C2	M12 x 130 Ø12	34	H	50	200
AP08095	-	M8 x 95 Ø8	29	E	100	600	AP12150	C1&C2	M12 x 150 Ø12	54	I	50	100
AP08115	-	M8 x 115 Ø8	49	G	100	400	AP12180	C1&C2	M12 x 180 Ø12	84	L	50	150
AP10090	C1	M10 x 90 Ø10	10	E	100	400	AP12200	C1&C2	M12 x 200 Ø12	104	M	50	150
AP10105	C1	M10 x 105 Ø10	25	F	50	300	AP16145	C1&C2	M16 x 145 Ø16	28	I	25	100
AP10115	C1	M10 x 115 Ø10	35	G	50	200	AP16175	C1&C2	M16 x 175 Ø16	58	K	25	50
AP10135	C1	M10 x 135 Ø10	55	H	50	200	AP16220	C1&C2	M16 x 220 Ø16	103	O	25	50
AP10165	C1	M10 x 165 Ø10	85	K	50	200	AP16250	C1&C2	M16 x 250 Ø16	133	Q	25	50
AP10185	C1	M10 x 185 Ø10	105	L	50	150	AP20170	-	M20 x 170 Ø20	32	K	20	40
• AP12080	-	M12 x 80 Ø12	4	D	50	300	AP20200	-	M20 x 200 Ø20	62	M	20	40
AP12100	C1&C2	M12 x 100 Ø12	4	E	50	200	AP24205	-	M24 x 205 Ø24	35	N	10	30
AP12110	C1&C2	M12 x 110 Ø12	14	F	50	200	AP24235	-	M24 x 235 Ø24	65	P	10	20

• Non assessed sizes. Resistance values and installation data are not applicable to these references. For further information, please contact Technical Department.